





Analog Inputs

- ±10 Vdc current reference
- Peak, continuous current & peak-time set

Analog Outputs

- Current monitor
- Current reference

Digital Inputs

- Amp Enable
- Fwd/Rev Enable (limit switches)
- Hi/Lo load inductance

Digital Outputs

- Amp OK
- Regen control
- Brake control

Feedback

• Digital Halls from brushless motors

Dimensions

- 53.3 x 45.7 x 15.2 mm
- 2.1 x 1.8 x 0.6 in



Actual Size

Model	Vdc	Ic	Ip
BTM-055-20	12~55	10	20
BTM-090-10	20~90	5	10



DEVELOPMENT KIT

DESCRIPTION

Bantam is a compact, DC powered analog current amplifier for torque control of DC brush or brushless motors. It operates as a stand-alone driver taking a $\pm 10V$ input from an external controller. Mounting to a PC board with solderless connectors facilitates lowcost, multi-axis designs.

The Amp Enable input interfaces to active LO signals up to 24 Vdc. Another digital input switches the current-loop gain from a high to low for load inductance compensation. Forward and Reverse Enable inputs are provided for limit switches.

A digital output for Amp-OK indicates the amplifier's status. There are two other digital outputs one of which can activate an external regenerative energy dissipator circuit and another for motor brake control.

Digital Hall feedback enables trapezoidal drive of DC brushless motors. For driving DC brush motors, these inputs are left unconnected and the motor connected between the U & V outputs.

Protections include I2T current limiting for peak and continuous current as well as peak time. Short circuits between outputs or to ground and amplifier over-temperature produce latching faults.

A Development Kit is available that provides mounting and easy connectivity for the Bantam.



GENERAL SPECIFICATIONS

Test conditions: Load = Wye connected load: 2 mH + 2 Ω line-line. Ambient temperature = 25°C, +HV = HV_{max}

MODEL	BTM-055-20	BTM-090-10		
OUTPUT POWER				
Peak Current	20	10	Adc, ±5%	
Peak time	1	1	Sec	
Continuous current	10	5	Adc, ±5%	
Peak Output Power	1045	855	W	
Continuous Output Power	523	427	W	
Output resistance	0.075	0.075	Rout (Ω)	
Maximum Output Voltage	Vout = $HV*0.97 - Rout*$	Iout		
NPUT POWER				
HV_{min} to HV_{max}	+12 to +55	+20 to +90	Vdc, Transformer-isolated	
Ipeak	20	10	Adc (1 sec) peak	
Icont	10	5	Adc continuous (Note 1)	
WM OUTPUTS				
Туре	3-	phase MOSFET, 33 kHz		
Commutation		dal using digital Hall fee	dback	
CONTROL				
Analog Reference Input	±10 Vdc, 100 kΩ differential ir	put impedance		
Bandwidths	Current loop: 2.5 kHz typical,		tuning & load inductance	
Minimum load inductance	200 µH line-line			
EEDBACK				
Digital Halls	3, non-isolated, for brushless motor commutation			
	10 k Ω to +5 Vdc pull-up with 33 μs RC filter to 74HC14 Schmitt trigger			
Power	+5 Vdc @ 250 mA max. (J1-21, 22) to power Hall sensors or commutating encoder			
DIGITAL INPUTS				
Number	4			
[IN1] /Enable	Amplifier enable, LO active, HI	[disables		
/PosEnab, /NegEnab	Forward and reverse direction limit switch/enable inputs: HI will disable output current in direction			
Туре	74HC14 Schmitt trigger operation			
.,,,,	Vin-LO < 1.35 Vdc, Vin-HI >3	-	-	
			-	
			rating from +5 Vdc with RC filter on input	
[LoInd] Low Inductance	74HCT, Vil = 0.8 Vdc max, Vih	= 2.0 Vdc min, input v	oltage range 0 to +24 Vdc	
[LoInd] Low Inductance	74HCT, Vil = 0.8 Vdc max, Vih	= 2.0 Vdc min, input v		
ANALOG INPUTS	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta	= 2.0 Vdc min, input v	oltage range 0 to +24 Vdc	
ANALOG INPUTS Number	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta	= 2.0 Vdc min, input v nce loads, LO or ground	oltage range 0 to +24 Vdc	
ANALOG INPUTS Number Ref(+), Ref(-)	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur	ree 2.0 Vdc min, input v nce loads, LO or ground rent demand, ±10 Vdc	oltage range 0 to +24 Vdc ed: for lower inductance loads	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr	rent lemand, ±10 Vdc rent limit from 10~1009	oltage range 0 to +24 Vdc ed: for lower inductance loads 6 of rated peak current	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou	rent demand, ±10 Vdc rent limit from 10~1009 us current limit from 10	oltage range 0 to +24 Vdc ed: for lower inductance loads	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100%	rent demand, ±10 Vdc rent limit from 10~1009 s current limit from 10~1009 s current limit from 10-	oltage range 0 to +24 Vdc led: for lower inductance loads % of rated peak current ~100% of rated continuous current	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100%	rent demand, ±10 Vdc rent limit from 10~1009 s current limit from 10~1009 s current limit from 10-	oltage range 0 to +24 Vdc ed: for lower inductance loads 6 of rated peak current	
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ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100% ±2.5 Vdc from the 2.5 Vdc qui	rent demand, ±10 Vdc rent limit from 10~100% us current limit from 10~100% of I2T time iescent state will adjust	oltage range 0 to +24 Vdc led: for lower inductance loads % of rated peak current ~100% of rated continuous current	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100% ±2.5 Vdc from the 2.5 Vdc qui	rent demand, ±10 Vdc rent limit from 10~1009 us current limit from 10~1009 us current limit from 106 of 12T time iescent state will adjust	oltage range 0 to +24 Vdc led: for lower inductance loads 6 of rated peak current ~100% of rated continuous current output current ±1% of peak rated current MA max for [AOK] and [OUT1], 1000 mA for [OUT2]	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance DIGITAL OUTPUTS Number: type	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100% ±2.5 Vdc from the 2.5 Vdc qui 3: N-channel MOSFET, open-d	rent demand, ±10 Vdc rent limit from 10~1009 is current limit from 10 of 12T time iescent state will adjust lrain, 30 Vdc max, 100 ifier has no faults and v	oltage range 0 to +24 Vdc led: for lower inductance loads 6 of rated peak current ~100% of rated continuous current output current ±1% of peak rated current mA max for [AOK] and [OUT1], 1000 mA for [OUT2] vill operate when enabled	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance DIGITAL OUTPUTS Number: type [AOK]	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100% ±2.5 Vdc from the 2.5 Vdc qui 3: N-channel MOSFET, open-d Amp OK: active LO when ampl Configured as external regen s	rent demand, ±10 Vdc rent limit from 10~1009 us current limit from 10~1009 is current limit from 10 of 12T time iescent state will adjust lrain, 30 Vdc max, 100 ifier has no faults and v witch controller: will be	oltage range 0 to +24 Vdc led: for lower inductance loads 6 of rated peak current ~100% of rated continuous current output current ±1% of peak rated current mA max for [AOK] and [OUT1], 1000 mA for [OUT2] vill operate when enabled	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance DIGITAL OUTPUTS Number: type [AOK] [OUT1] [OUT2]	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100% ±2.5 Vdc from the 2.5 Vdc qui 3: N-channel MOSFET, open-d Amp OK: active LO when ampl Configured as external regen s	rent demand, ±10 Vdc rent limit from 10~1009 us current limit from 10~1009 is current limit from 10 of 12T time iescent state will adjust lrain, 30 Vdc max, 100 ifier has no faults and v witch controller: will be	oltage range 0 to +24 Vdc led: for lower inductance loads 6 of rated peak current ~100% of rated continuous current output current ±1% of peak rated current mA max for [AOK] and [OUT1], 1000 mA for [OUT2] vill operate when enabled LO to turn on regen switch	
ANALOG INPUTS Number Ref(+), Ref(-) Peak Current Limit Continuous Current Limit I2T Limit Balance DIGITAL OUTPUTS Number: type [AOK] [OUT1]	74HCT, Vil = 0.8 Vdc max, Vih HI or open: for higher inducta 5 Command input for output cur 0.5 to 4.80 Vdc sets peak curr 0.5 to 4.87 Vdc sets continuou 0.5 to 5.00 Vdc sets 10~100% ±2.5 Vdc from the 2.5 Vdc qui 3: N-channel MOSFET, open-d Amp OK: active LO when ampl Configured as external regen s	rent demand, ±10 Vdc rent limit from 10~1009 us current limit from 10~1009 is current limit from 10 of 12T time iescent state will adjust lrain, 30 Vdc max, 100 ifier has no faults and v witch controller: will be	oltage range 0 to +24 Vdc led: for lower inductance loads 6 of rated peak current ~100% of rated continuous current output current ±1% of peak rated current mA max for [AOK] and [OUT1], 1000 mA for [OUT2] vill operate when enabled LO to turn on regen switch	

NOTES

1) Heatsink is required for continuous current rating.

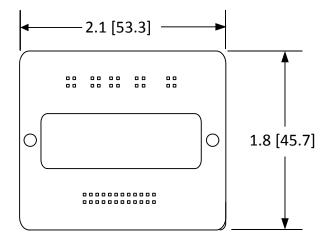




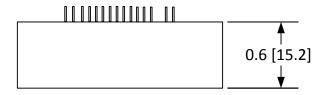


MOTOR CONNECTIONS	
Phase U, V, W Hall U, V, W Hall power	PWM outputs to 3-phase ungrounded Wye or delta wound brushless motors, or DC brush motors (U-V) Digital Hall signals, single-ended +5 Vdc ±2% @ 250 mAdc max
PROTECTIONS	
HV Overvoltage	+HV > HV _{max} , Amplifier outputs turn off until +HV < HV _{max} (See Input Power for HV)
HV Undervoltage	BTM-090-10: +HV < +20 Vdc, Amplifier outputs turn off until +HV > +20 Vdc
	BTM-055-20: +HV < +12 Vdc, Amplifier outputs turn off until +HV > +12 Vdc
Amplifier over temperature	Heat plate > 70°C
Short circuits	Output to output, output to ground, internal PWM bridge faults
I ² T Current limiting	Programmable: continuous current, peak current, peak time
MECHANICAL & ENVIRONMENTA	L
Size	2.1 x 1.8 x 0.6 [53.3 x 45.7 x 15.2] in [mm]
Weight	Amplifier: 0.082 lb [0.037 kg], heatsink 0.113 lb [.051 kg]
Ambient temperature	0 to +45 °C operating, -40 to +85 °C storage
Humidity	0 to 95%, non-condensing
Contaminants	Pollution degree 2
Environment	IEC68-2: 1990
Cooling	Conduction through heatplate on amplifier chassis, or convection

AMPLIFIER DIMENSIONS



Dimensions in inches [mm]







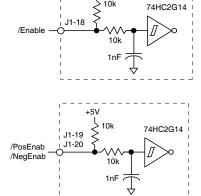
CONTROL INPUTS AND OUTPUTS

ENABLE INPUT

The Enable input [IN1] is LO-active and pulled up to +5V by an internal 10k resistor. This provides fail-safe operation by disabling the amplifier if the Enable input is open, or a wire from the controller should break.

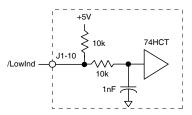
FWD/REV ENABLE INPUTS

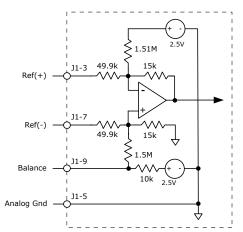
Two inputs are provided for limit switches. These should be LO for normal operation, and open or HI to inhibit current of positive or negative polarity.



+5V

10k





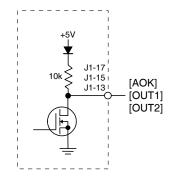


The output current of the amplifier can be adjusted to 0 Adc by connecting the balance input to a potentiometer with an adjustment range of 0 to +5 Vdc. This will produce an offset adjustment range of $\pm 0.8\%$ of the Ipeak rating of the amplifier. The table below shows the offset adjustment range in mA.

Model	±Ioffset (mA)
BTM-055-20	160
BTM-090-10	80

DIGITAL OUTPUTS

Three N-channel MOSFETs sink current from loads connecting to +30 Vdc maximum. Outputs [AOK] and [OUT1] can sink 100 mA maximum. The brake output [OUT2] can sink 1000 mA. An external flyback diode is required with driving inductive loads like a brake, or relays.



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LOAD INDUCTANCE INPUT

ANALOG REFERENCE INPUT

analog signal from an external controller.

The /LowInd input controls the gain of the current error amplifier to compensate the amplifier for lower or higher inductance loads. With the input open, the bandwidth will be ~2.5 kHz for a 2 mH (line-line) load. Grounding the input reduces the gain to 1/10 of the input-open gain for the same bandwidth with 200 μ H loads.

The amplitude and polarity of the amplifier output current is controlled by a $\pm 10V$





MOTOR CONNECTIONS

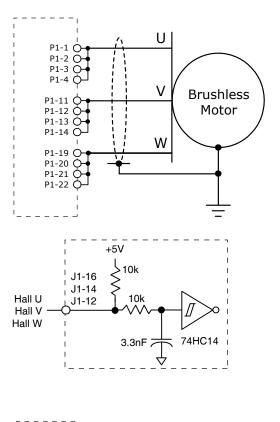
Motor connections are of two types for brushless motors: phases and Halls. For brush motors, only the armature connections are needed. The phase or armature connections carry the amplifier output currents that drive the motor to produce motion. The Hall signals are three digital signals used for commutating a brushless motor. When using a brush motor the Hall inputs should be unconnected and the motor armature connections made between the U & V phase outputs.

MOTOR PHASING: BRUSHLESS

Phasing can be done simply by connecting the motor Halls and phase wires to the BTM based on their signal names. Then, enable the amp and use the Offset adjust pot as a reference source by removing JP1-A. There are six possible combinations of the UVW phase wires and only one will produce torque correctly. If the UVW motor phase connection doesn't work, the other five combinations can be found easily by swapping two wires at a time: swap UV, swap VW, swap WU, swap UV, swap VW. Only one combination will produce smooth torque equally in both directions of rotation. Once the correct connection is found, check the direction of rotation. If it's desireable to reverse the direction of rotation, swap the U & W Halls, and swap the U & W motor phases.

MOTOR PHASE CONNECTIONS: BRUSHLESS

The amplifier output is a three-phase PWM inverter that converts the DC buss voltage (+HV) into DC voltage waveforms that drive two motor phase-coils at a time (trapezoidal commutation). Cable should be sized for the continuous current rating of the amplifier. Motor cabling should use twisted, shielded conductors for CE compliance, and to minimize PWM noise coupling into other circuits. The motor cable shield should connect to motor frame and the equipment frame ground for best results.

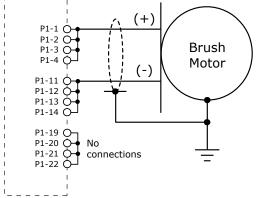


MOTOR HALL SIGNALS: BRUSHLESS

Hall signals are single-ended signals that provide absolute feedback within one electrical cycle of the motor. There are three of them (U, V, & W) and they may be sourced by magnetic sensors in the motor, or by encoders that have Hall tracks as part of the encoder disc. They typically operate at much lower frequencies than the motor encoder signals, and are used for commutation. When driving DC brush motors, the Hall inputs should be left unconnected.

MOTOR PHASE CONNECTIONS: BRUSH

The amplifier output is an H-bridge PWM inverter that converts the DC bus voltage (+HV) into a DC voltage waveform that drives the motor armature. Cable should be sized for the continuous current rating of the amplifier. Motor cabling should use twisted, shielded conductors for CE compliance, and to minimize PWM noise coupling into other circuits. The motor cable shield should connect to motor frame and the equipment frame ground for best results.







CURRENT LIMIT INPUTS

Two inputs are provided for setting the peak and continuous current limits. The I-Peak and I-Cont inputs each have equivalent circuits shown below. Limits can be set either by applying a voltage (Vset) to the input or by connecting a resistor (Rset) between input and signal ground. The tables below show values for Rset and Vset that give 10~100% of the rated peak and continuous current ratings.

AMPLIFIER MODELS AND RATINGS

Model	I-Peak	I-Cont	T-Peak	I2T
BTM-055-20	20	10	1	300
BTM-090-10	10	5	L	75

Note: I2T = (Ipeak² - Icont²) * T-peak

PEAK CURRENT LIMIT SETTINGS

%	Vpeak	Rpeak
100	4.80	<0UT>
90	4.32	86400
80	3.84	38400
70	3.36	22400
60	2.88	14400
50	2.4	9600
40	1.92	6400
30	1.44	4114
20	0.96	2400
10	0.48	1067

To use the table, find the % value as follows:

% = NewPeakCurrent * 100

AmpPeak Current

CONTINUOUS CURRENT LIMIT SETTINGS

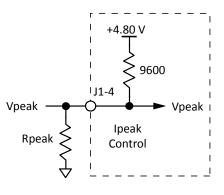
%	Vcont	Rcont
100	4.87	<0UT>
90	4.38	88189
80	3.90	39195
70	3.41	22864
60	2.92	14698
50	2.44	9799
40	1.95	6533
30	1.46	4199
20	0.97	2450
10	0.49	1089

To use the table, find the % value as follows:

% = <u>NewContCurrent * 100</u>

AmpContCurrent

EQUIVALENT CIRCUIT



EQUIVALENT CIRCUIT

^IJ1-6

Vcont

Rcont

4.87 V

Icont

Control

9799

Vcont

EXAMPLE I-Peak SETTING

If a voltage Vpeak is used to control the peaklimit current, it can be found like this: Vpeak = 4.80 * NewPeakCurrent

AmpPeakCurrent

Example: find Vpeak for a 6 A NewPeakCurrent using a BTM-090-10: Vpeak = 4.80 * 6 = 2.88 V

To use a resistor for setting Peak-Limit current, calculate the value as follows:

Rpeak = 9600 * NewPeakCurrent

(AmpPeakCurrent - NewPeakCurrent)

Example: find Rpeak for a 6 A PeakLimitCurrent:

Rpeak = $\frac{9600 * 6}{(10 - 6)}$ = 14,400 ohms

EXAMPLE Icont SETTING

If a voltage Vcont is used to control the peak-limit current, it can be found like this:

Vcont = 4.87 * NewContCurrent
AmpContCurrent

Example: find Vcont for a 3 A NewContCurrent using a BTM-090-10: Vcont = 4.87 * 3 = 2.92 V

5

To use a resistor for setting Cont-Limit current, calculate the value as follows:

Rcont = 9799 * NewContCurrent

(AmpContCurrent - NewContCurrent)

Example: find Rcont for a 2 A NewContCurrent:

Rcont =
$$\frac{9799 * 2}{(5 - 2)}$$
 = 6,533 ohms

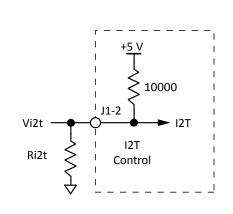




PWM LIMITING INPUT

12T LIMIT SETTINGS

%	Vi2t	Ri2t
100	5.0	<0UT>
90	4.50	90000
80	4.00	40000
70	3.50	23333
60	3.00	15000
50	2.50	10000
40	2.00	6667
30	1.50	4286
20	1.00	2500
10	0.50	1111



EQUIVALENT CIRCUIT

12T LIMITS (AMP²·SECS) OF AMPLIFIERS

I2T Limit = (Ipeak^2 - Icont^2) * 1 sec Model I2T Limit BTM-055-20 300 BTM-090-10 75

EXAMPLES OF 12T SETTINGS

- I2T Limit settings should be made after the peak and continuous current limits have been set. The time that the peak current can be maintained is then calculated based on the amplifier model and the new peak/continuous current limit settings. If a shorter peak time is desired, a new I2T Limit can be produced with an external voltage or resistor as described below.
- Example 1: Find a the I2T limit for a BTM-055-20 with peak/continuous currents set to 12 & 9 A and a new peak time of 0.5 s
 - 1) I2T Limit for BTM-055-20 = Amp I2T $A^2 \cdot s = (20^2 10^2)A^{2*1} \sec = 300 A^2 \cdot s$ 2) Find new I2T A^2 for 12/9 limits = $(12^2 9^2)A^2 = 63 A^2$

 - 3) Find new peak time = Amp I2T A^2 s / New I2T A^2 , or 300 / 63 = 4.76 s

Example 2: Select an external resistor to shorten the peak I2T time for the peak/continuous current limits in Example 1 using the pre-set peak/cont current limits and a new desired peak time of 0.5 secs.

- 1) Calculate the new I2T Limit in $A^2 \cdot s = (12^2 6^2) * 0.5$ sec = 54 $A^2 \cdot s$
- 2) Find the ratio of the new I2T Limit to the amplifier I2T limit: (54 / 300) = 0.18, or 18%
- 3) Using the table above, find the nearest entry to 18% and install an external Ri2t with the table value
- 18% is close to 20%, and the table gives a value of 2500 ohms (2.5k) for this.
- 4) Or, calculate a resistor value that gives the exact new peak time desired:
- Ri2t = 10000 * X / (1-X) where X = ratio of the new I2T Limit to the amplifier I2T limit (54 / 300) Ri2t = 10000 * 0.18 / (1-0.18) = 2195 ohm. A 2.2k, 1% resistor is close to this value.
- 5) To find a voltage that can be applied to J1-2 to produce the same effect, multiply 5.0V X the ratio of I2T limits (54 / 300)
- 5.0 X (54 / 300) = 0.90 Vdc.

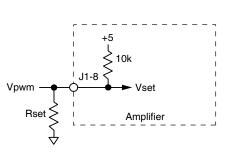
ABOUT PWM LIMITING

PWM limiting sets a maximum value for the on vs. off time of the outputs of the amplifier. While the peak voltage seen by the load remains about the same as the supply voltage (HV), the average voltage seen by the motor can be limited. A common use of this is to limit the maximum RPM of a motor even though it's operating in torque mode.

PWM LIMIT SETTINGS

%	Rset (K)	Vset
97	<0UT>	4.95
78	42	4.00
70	30	3.71
68	25	3.54
62	20	3.3
57	15	2.97
45	10	2.48
38	7.5	2.12
28	5	1.65
25	2.5	0.99
25	0	0

EQUIVALENT CIRCUIT



EXAMPLE PWM SETTING

The table shows duty cycles measured with some choices of Rset for the PWM limits.



Trapezoidal Torque Amplifier Module



PC BOARD DESIGN

Printed circuit board layouts for Bantam amplifiers should follow some simple rules:

1. Install a low-ESR electrolytic capacitor not more than 12 inches from the drive. PWM amplifiers produce ripple currents in their DC supply conductors. Bantam amplifiers do not use internal electrolytic capacitors as these can be easily supplied by the printed circuit board. In order to provide a good, low-impedance path for these currents a low-ESR capacitor should be mounted as close to the drive as possible. 330 μ F is a minimum value, with a voltage rating appropriate to the drive model and power supply.

2. Connect P1 signals (U,V,W outputs, +HV, and +HV Common) in pin-groups for current-sharing. The signals on P1 are all high-current types (with the exception of the +24 Vdc Aux HV supply). To carry these high currents (up to 20 Adc peak) the pins of P1 must be used in multiples to divide the current and keep the current carrying capacity of the connectors within specification. The diagram on page 9 shows the pin groups that must be inter-connected to act as a single connection point for pc board traces.

3. Follow IPC-2221 rules for conductor thickness and minimum trace width of P1 signals. The width and plating should depend on the model of drive used, the maximum voltage, and maximum current expected to be used for that model. Power supply traces (+HV, +HV Common) should be routed close to each other to minimize the area of the loop enclosed by the drive DC power. Noise emission or effects on nearby circuitry are proportional to the area of this loop, so minimizing it is good layout practice.

Motor signals (U,V,W) should also be routed close together. All the motor currents sum to zero, and while the instantaneous value in a given phase will change, the sum of currents will be zero. So, keeping these traces as closely placed as possible will again minimize noise radiation due to motor phase currents.

Bantam circuit grounds are electrically common, and connect internally. However, the P1 signals carry high currents while the grounds on J1 (signal ground) carry low currents. So, J1 signals should be routed away from, and never parallel to the signals on P1. Encoder signal pairs (A, /A, B, /B, and X, /X) should be routed close together for good transmission-line effect to reduce reflections and noise.

The amplifier heatplate is electrically isolated from all drive circuits. For best noiseimmunity it is recommended to connect the standoffs to frame ground and to use metal mounting screws to maintain continuity between heatplate and standoffs.



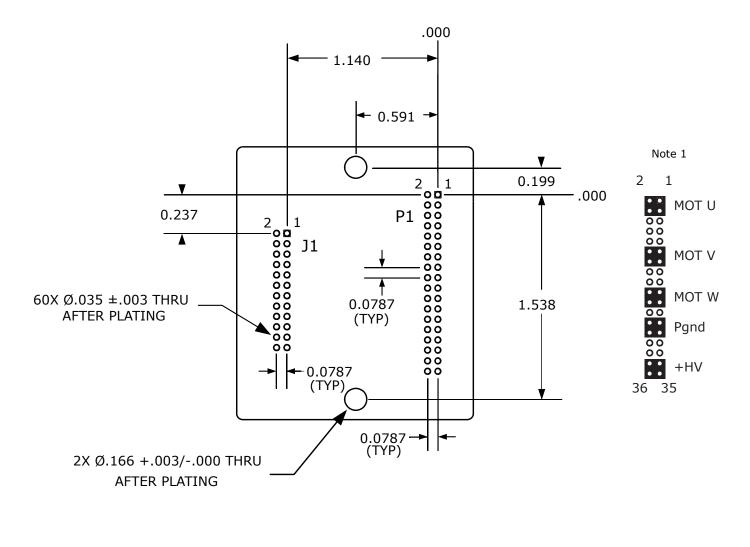
Trapezoidal Torque Amplifier Module



PC BOARD MOUNTING FOOTPRINT

Top View

Dimensions in inches



Accelnet Mounting Hardware:

Qty	Description	Mfgr	Part Number	Remarks
1	Socket Strip	Samtec	SQW-112-01-L-D	J1
1	Socket Strip	Samtec	SQW-118-01-L-D	P1

Notes

1. P1 signals must be connected for current-sharing.

2. To determine copper width and thickness for P1 signals refer to specification IPC-2221.

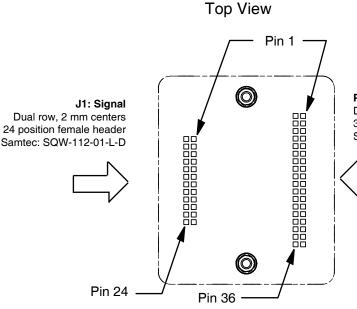
(Association Connecting Electronic Industries, http://www.ipc.org)

3. Standoffs should be connected to etches on pc board that connect to frame ground for maximum noise suppression and immunity.





AMPLIFIER PC BOARD CONNECTORS



Drive viewed from above looking down on the pc board on which it is mounted.

Pins shown in grey are unused locations in PC board socket

P1: Motor & HV Dual row, 2 mm centers 36 position female header Samtec: SQW-118-01-L-D

J1 SIGNALS & PINS

Signal	P	in	Signal
I2T Time	2	1	Current Ref
Peak Curr Limit	4	3	Ref(+)
Cont Curr Limit	6	5	Agnd
PWM Limit	8	7	Ref(-)
/LowInd	10	9	Balance
Hall W	12	11	Current Monitor
Hall V	14	13	[OUT2]
Hall U	16	15	[OUT1]
/Enable	18	17	[AOK]
/NegEnab	20	19	/PosEnab
Hall +5V	22	21	Hall +5V
Pgnd	24	23	Pgnd

P1 SIGNALS & PINS

Signal	Р	in	Signal
Motor U	2	1	Motor U
Motor U	4	3	Motor U
N/C	6	5	N/C
N/C	8	7	N/C
N/C	10	9	N/C
Motor V	12	11	Motor V
Motor V	14	13	Motor V
N/C	16	15	N/C
N/C	18	17	N/C
Motor W	20	19	Motor W
Motor W	22	21	Motor W
N/C	24	23	N/C
Pgnd	26	25	Pgnd
Pgnd	28	27	Pgnd
N/C	30	29	N/C
N/C	32	31	N/C
+HV	34	33	+HV
+HV	36	35	+HV

NOTES

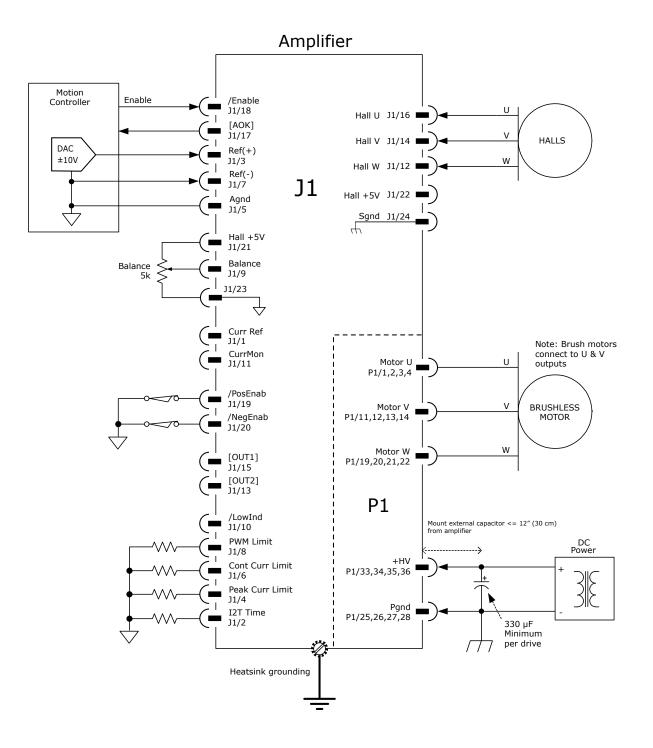
- 1. Grey-shaded signal are N.C. (No Connection)
- 2. Signals are grouped for current-sharing on the power connector. When laying out pc board art-
- works, all pins in groups having the same signal name must be connected.
- 3. Total output current from +5V pins (J1-21,22) cannot exceed 250 mA.







AMPLIFIER CONNECTIONS



NOTES

- 1. Total output current from +5V pins (J1-21,22) cannot exceed 250 mA.
- 2. When Balance potentiometer is used, it should connect to amplifier +5V and ground for best stability.





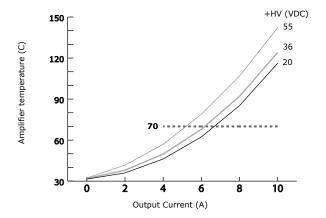
AMPLIFIER TEMPERATURE VS OUTPUT CURRENT AND HV AT 25C AMBIENT

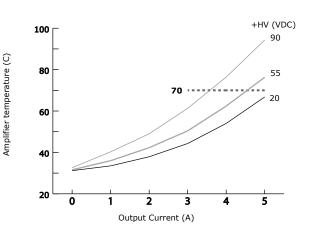
The curves below use the amplifier power dissipation information and the thermal resistance of 12 °C/W without any heatsink or forced-air cooling to show quickly if a heatsink or forced-air cooling will be required.

When output current is known, draw a vertical line to the curve of the supply voltage (HV) that's closes to the HV in use and mark the spot where they intersect. If the point is above the 70C line on the chart, then either a heatsink or forced-air cooling will be required. If this is the case, then use the following curves for power dissipation and thermal resistance to determine what combination of heatsinking and/or cooling would be required.

BTM-055-20



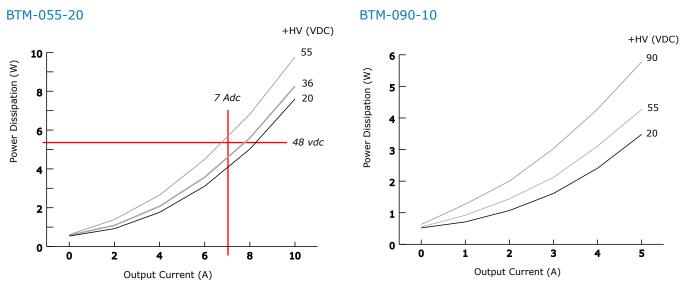




HEATSINK AND FORCED-AIR COOLING: HOW TO FIND OUT IF THESE ARE REQUIRED

To see if a heatsink or fan-cooling is required, find the temperature rise the drive will experience when it's installed. For example, if the ambient temperature in the drive enclosure is 40 °C, and the heatplate temperature is to be limited to 70° C or less to avoid shutdown, the maximum rise would be 70C - 40C. or 30C. Then find the power dissipation in the charts below. Divide the temperature rise by the power dissipation and the result is thermal resistance in °C/W. Find this value on the Y-axis of the charts on the following page and draw horizontal lines across the charts to show what combinations of heatsink and air movement will produce this thermal resistance.

POWER DISSIPATION VS. OUTPUT CURRENT AND HV



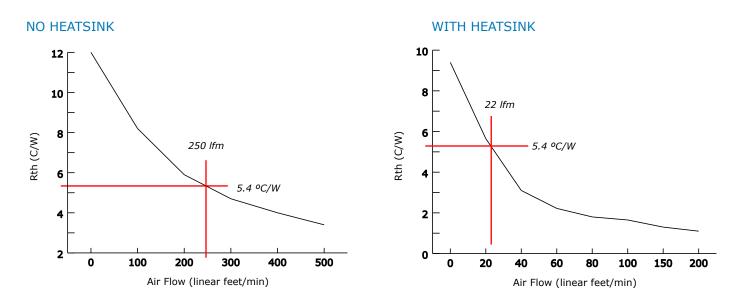
Copley Controls, 20 Dan Road, Canton, MA 02021, USA Tel: 781-828-8090 Tech Support: E-mail: sales@copleycontrols.com, Internet: http://www.copleycontrols.com Fax: 781-828-6547 Page 12 of 18





THERMAL RESISTANCE

The temperature rise of the amplifier when operating depends on the power dissipation and the thermal resistance between the amplifier and the environment.



EXAMPLE

A BTM-055-20 application needs to output 7 Adc while operating from a 48 V power supply. In the chart on p. 10, place a vertical line at the 7 Adc point. Next draw a horizontal line that intersects it at a point 2/3 of the way between the 36 & 55 V curves, estimating a 48 Vdc power supply. This line yields a power dissipation of 5.4 W. Next, draw lines at the 5.4 $^{\circ}$ C/W point on the curves above. These show that adding a heatsink reduces the air circulation requirement from 250 lfm to ~25 lfm. This low value can probably be met using a single fan in the enclosure to circulate air where it could cool multiple Bantam amplifiers adequately.

HEATSINK INSTALLATION

If a heatsink is used it is mounted using the same type of screws used to mount the drive without a heatsink but slightly longer. Phase change material (PSM) is used in place of thermal grease. This material comes in sheet form and changes from solid to liquid form as the drive warms up. This forms an excellent thermal path from drive heatplate to heatsink for optimum heat transfer.

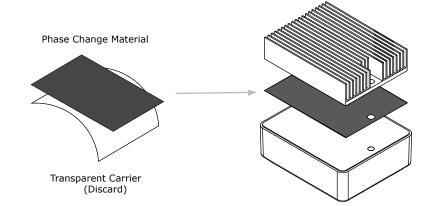
STEPS TO INSTALL

1. Remove the PSM (Phase Change Material) from the clear plastic carrier.

2. Place the PSM on the *Bantam* aluminum heatplate taking care to center the PSM holes over the holes in the drive body.

3. Mount the heatsink onto the PSM again taking care to see that the holes in the heatsink, PSM, and drive all line up.

4. Torque the #4-40 mounting screws to $8 \sim 10$ lb-in (0.9 ~ 1.13 N·m).



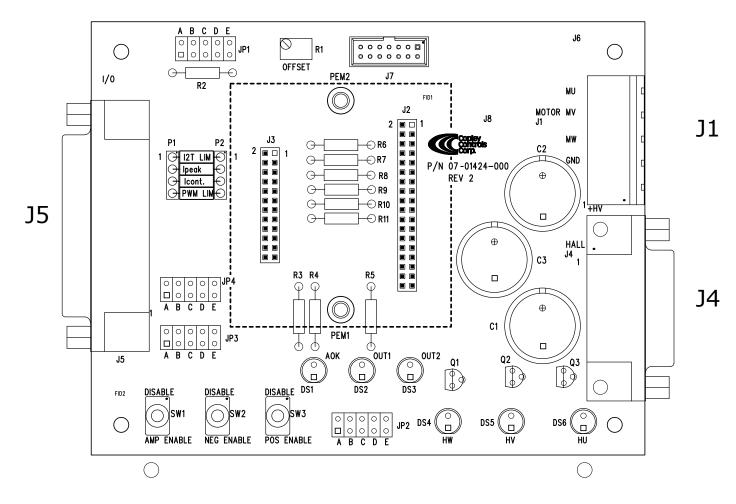




DEVELOPMENT KIT TOP VIEW

The graphic below shows the placement of components and connectors on the Development Kit PC board. The Bantam amplifier is not shown, but mounts in the outline that contains connectors J3 & J2.

Bantam



SOCKETED COMPONENTS

P1/P2	Remarks
1	I2T Time setting resistor
2	Ipeak setting resistor
3	Icont setting resistor
4	No function





These charts show the pins and signals for the Development Kit connectors.

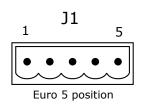
Bantam

J1 MOTOR AND HV POWER

Pin	Signal
5	Mot U
4	Mot V
3	Mot W
2	HV Gnd
1	+HV Input

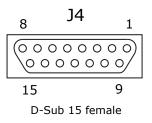
J4 HALLS

Signal	Pin		Signal
Sgnd	1	9	n.c.
Hall U	2	10	Sgnd
Hall V	3	11	+5 Vdc output
Hall W	4	12	Sgnd
Sgnd	5	13	n.c.
n.c.	6	14	n.c.
n.c.	7	15	n.c.
n.c.	8		



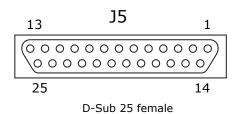
RoHS

BTM



J5 CONTROL

Signal	Р	in	Signal
Sgnd	1	14	Ref(-)
Ref(+)	2	15	Sgnd
Ext Balance	3	16	Sgnd
/NegEnab	4	17	/PosEnab
/Enable	5	18	Gain Select
[OUT1]	6	19	Sgnd
Current Cont Limit	7	20	n.c.
Current Ref	8	21	Curr Peak Limit
I2T Time	9	22	[AOK]
Current Monitor	10	23	+5 Vdc Output
[OUT2]	11	24	n.c.
Sgnd	12	25	n.c.
Sgnd	13		



NOTES

1) The combined current from J4-11 and J5-23 cannot exceed 250 mA.

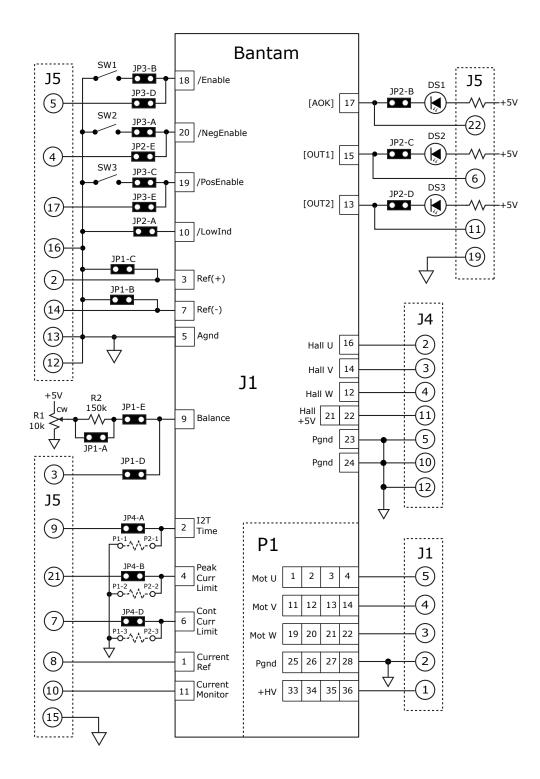




CONNECTIONS

In the diagram below, connectors inside the Bantam outline are the amplifier connectors, their signal names, and pin numbers. All connectors and components outside of the Bantam are on the Development Kit.

Bantam



NOTES

1) The combined current from J4-11 and J5-23 cannot exceed 250 mA.





JUMPER FUNCTIONS

The functions shown in the tables below are in effect when the jumper is in place. When a jumper is removed, the stated function is disabled. J5 connects to an external controller

Bantam

JP1

JP1	Remarks		
А	Shorts 150k balance scaler		
В	Ref(-) input is grounded		
С	Ref(+) input is grounded		
D	Connects J5-3 to Amp: Balance		
E	R1 controls Amp: Balance		

JP2

JP2	Remarks
Α	Gain Select to Sgnd
В	Amp: [AOK] drives DS1
С	Amp: [OUT1] drives DS2
D	Amp: [OUT2] drives DS3
E	Connects J5-4 to Amp: /NegEnab

JP3

JP3	Remarks
А	Connects SW2 to Amp: /NegEnab
В	Connects SW1 to Amp: /Enable
С	Connects SW3 to Amp: /PosEnab
D	Connects J5-5 to Amp: /Enable
E	Connects J5-17 to Amp: /PosEnab

JP4

JP4	Remarks
А	Connects J5-9 to Amp: I2T Time
В	Connects J5-21 to Amp: Current Peak Limit
С	No connections
D	Connects J5-7 to Amp: Current Cont Limit
E	Connects J5-18 to Amp: Gain Select





MASTER ORDERING GUIDE

BTM-055-20	Bantam analog current amplifier, 10/20 Adc
BTM-090-10	Bantam analog current amplifier, 5/10 Adc
BDK-090-01	Development kit
BDK-CK	Connector Kit for Development Kit

ORDERING EXAMPLE

Example: Order 1 BTM-055-20 current amplifier and development kit:

<u>Qty</u>	<u>Item</u>	<u>Remarks</u>

- 1BTM-055-20Bantam current amplifier1BDK-090-01Development Kit for Bantam amplifier2Development Kit for Bantam amplifier
- 1 BDK-CK Connector Kit for Development Kit

ACCESSORIES

ORDER NUMBER	Qty	Ref	DESCRIPTION
BDK-CK Connecto	or kit fo	or BDK	-090-01 Development Kit (includes next 5 items shown below)
	1	J1	Connector, RoHS, Euro style plug, 5 position, Tyco (AMP) 796635-5
	1	J4	Connector, D-Sub, 15-position, male, RoHS, Tyco (AMP) 5-747908-2
	1 J4		Backshell, D-Sub, RoHS, metallized, 15-position, Norcomp 979-015-020R121
	1	J5	Connector, D-Sub, 25-position, male, RoHS, Tyco (AMP) 5-747912-2
	1	J5	Backshell, D-Sub, RoHS, metallized, 25-position, Norcomp 979-025-020R121

HEATSINK (OPTIONAL)

Heatsink Kit BTM-HK	1	Heatsink kit (for field-installation by customer)
	1	Heatsink Thermal Phase-change Material
	4	Heatsink hardware (#4-40 screws)